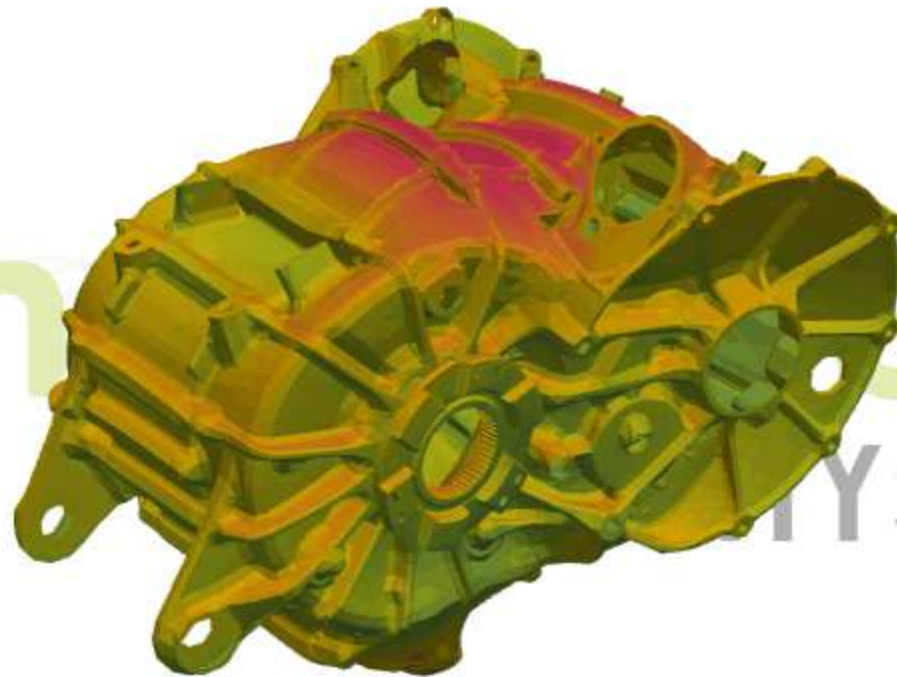


10 Common Misconceptions on Magnetic Noise & Vibrations (e-NVH)



Illustrated with Manatee e-NVH CAE collaborative platform developed by EOMYS

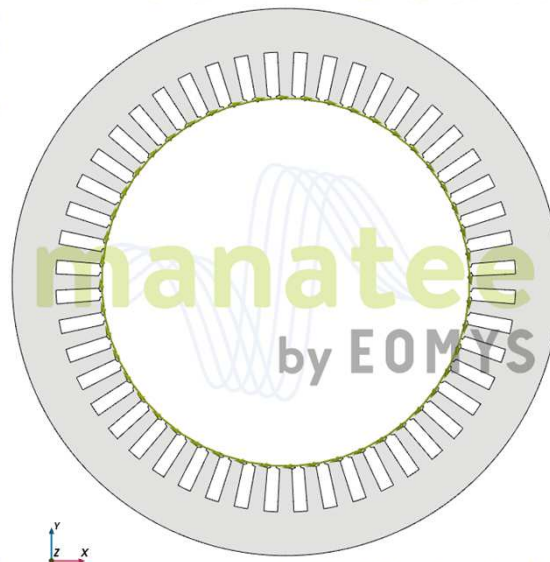
www.e-nvh.eomys.com

#1 « Magnetic noise and vibrations comes from torque ripple »

Torque ripple is generated by a small fraction of magnetic force harmonics (wavenumber $r=0$, tangential direction). Significant e-NVH levels can be produced by radial forces.

Besides, peak to peak metrics are not suitable for e-NVH as they combine phase information of different harmonics.

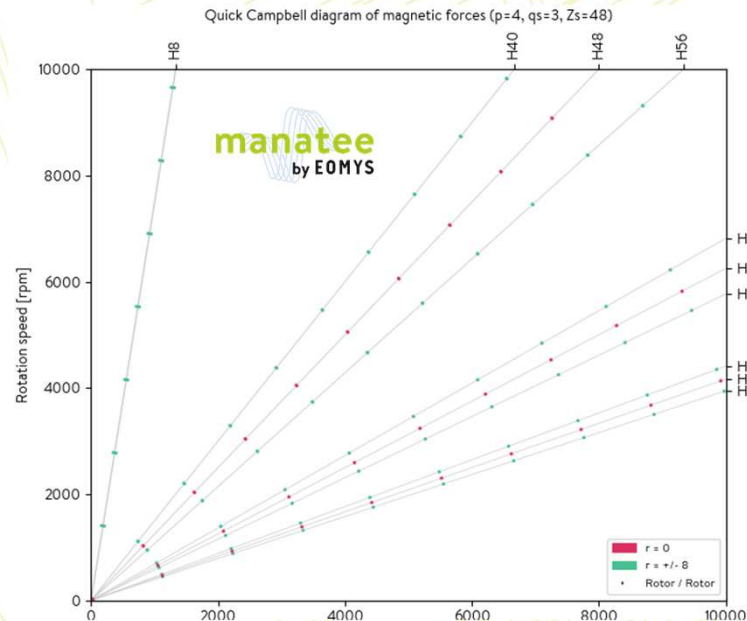
There is no general correlation between e-NVH and torque ripple levels according to EOMYS experience.



#2 « e-NVH problems can be avoided by choosing the right slot/pole combination »

Slot/pole combination gives an idea of the structure of the magnetic force spectrum, but for a same slot/pole combination quiet and noisy machines can be designed.

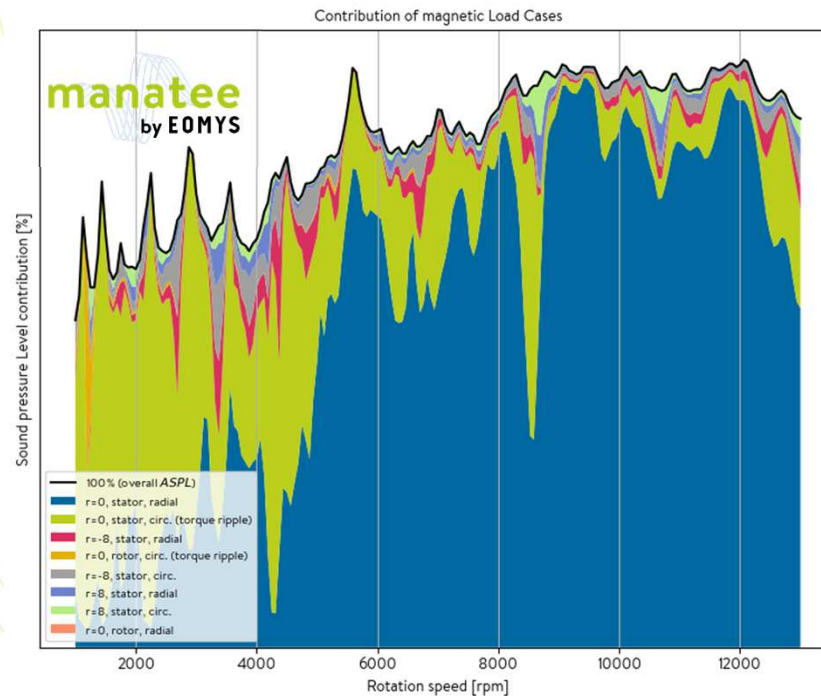
e-NVH level is influenced by stator/rotor natural frequencies so there can't exist a « quiet » slot/pole combination.



#3 « Airborne noise is produced by radial magnetic forces »

Stator normal deflections can be produced by tangential forces of positive wavenumbers. In some slot/pole combinations, tangential forces may produce as much airborne noise as radial forces.

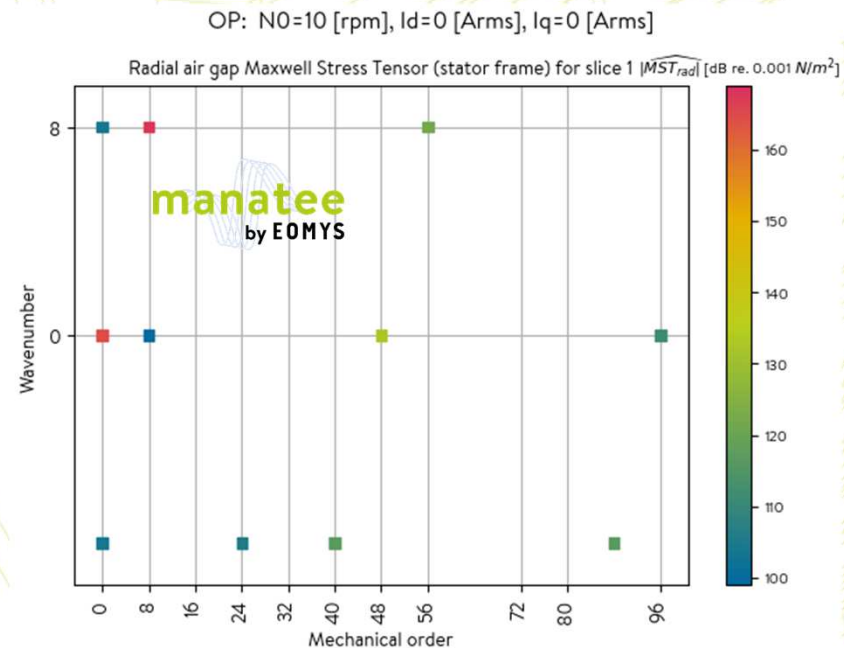
Torsional forces applied to external stator may induced bending deflections suitable to produce significant airborne noise.



#4 « Excitations can be analyzed through Maxwell stress harmonics wavenumber and frequencies »

Stator normal deflections can be produced by tangential forces of positive wavenumbers. In some slot/pole combinations, tangential forces may produce as much airborne noise as radial forces.

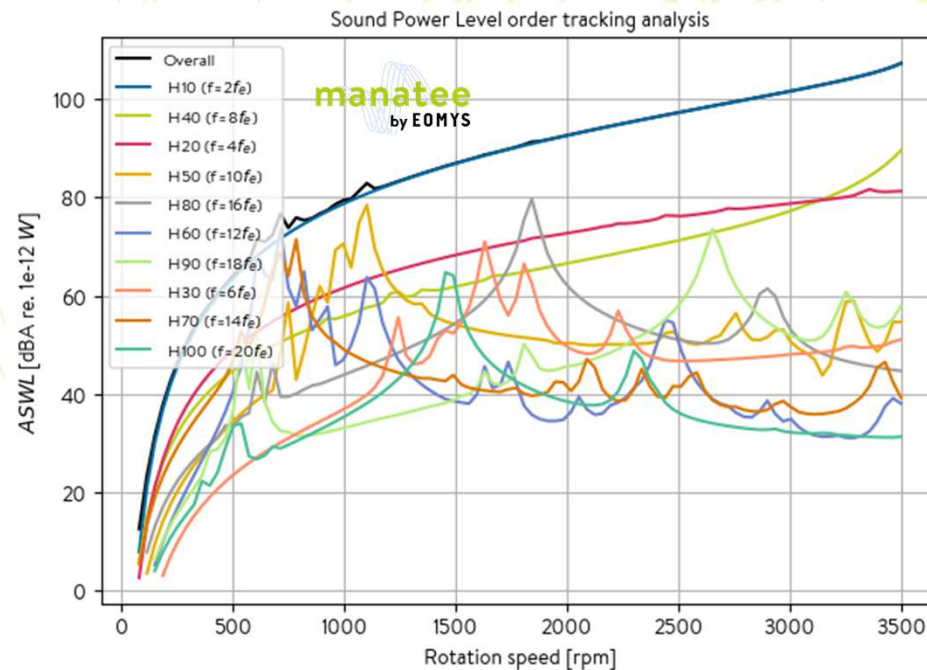
Torsional forces applied to external stator may induced bending deflections suitable to produce significant airborne noise.



#5 « High magnetic noise level comes from resonances between magnetic forces and structural modes »

Significant levels of magnetic noise and vibrations can be produced by forced excitation regime, in particular due to fundamental force at twice the electrical frequency.

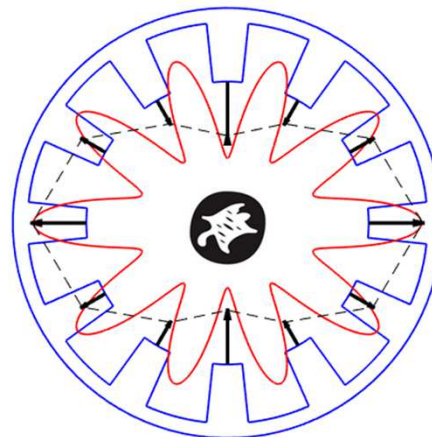
Switching noise can also produce significant noise without any particular resonance.



#6 « High e-NVH levels come from Maxwell stress harmonics with low wavenumber »

Maxwell stress harmonics are not physical local forces, they can only be used to reflect global forces (e.g. torque, UMP). It should therefore be analyzed carefully.

A modulation effect occurs when going from Maxwell stress to physical, local forces observed by stator teeth (« lumped forces »). This modulation effect may convert high wavenumber Maxwell stress harmonics into low wavenumber lumped forces.

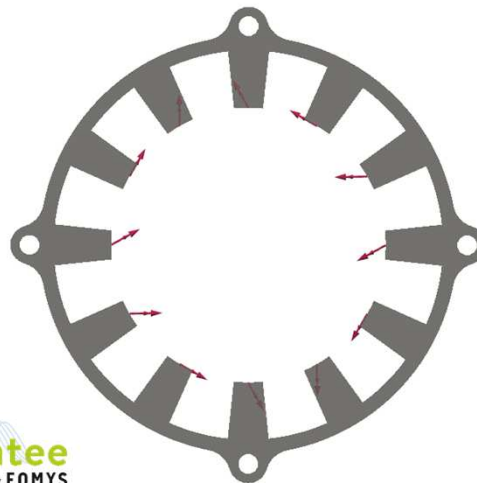


#7 « Lowest wavenumber of magnetic forces is given by $\text{GCD}(Z_s, 2p)$ in PMSM »

This formula on Greatest Common Divider is only true in open circuit, symmetrical machine (no eccentricity, no uneven airgap, no uneven magnetization) and holds for Maxwell stress harmonics, not physical harmonics observed by stator teeth.

Under load the formula is more complex as it depends on winding pattern. Wavenumbers of stator lumped forces include a modulation effect which is not taken into account in this formula.

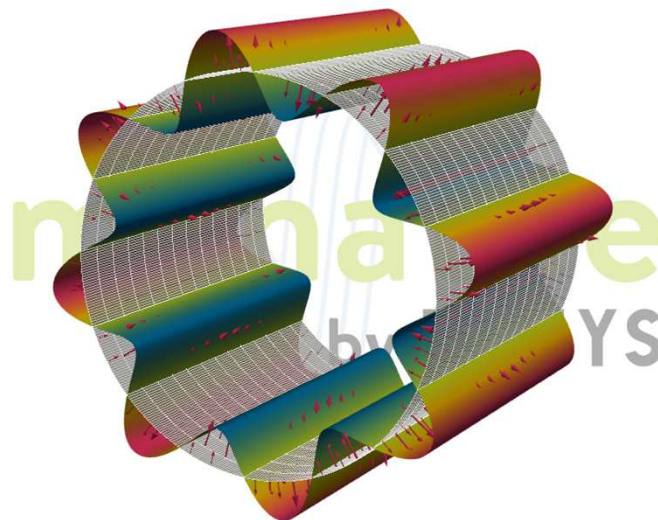
resultant OFS at N=750.3 rpm
f=125.05 Hz (Fmax=11.483 N)



#8 « Magnetic noise and vibrations are produced by low wavenumber forces »

« Low » wavenumber forces depends on the shape ratio of the lamination. In large electrical machines, EOMYS observed high magnetic noise levels with wavenumber $r=27$.

High vibration levels can be produced by high wavenumber forces due to fundamental field (e.g. $r=2p=8$ in a 8-pole traction IPMSM).

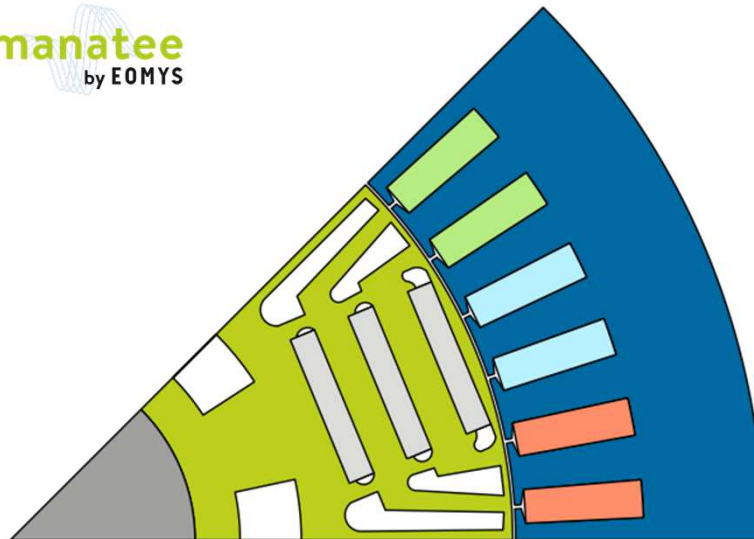


#9 « Closing the slot reduces magnetic noise and vibration »

Magnetic noise may not be produced by slotting effect. Some electromagnetic excitations come from fundamental field or winding harmonics, which are independent of slotting effects.

The decrease of slotting excitations with slot opening reduction is limited by magnetic saturation. Besides, some induction machine may show lower noise level when increasing slot opening depending on the initial design.

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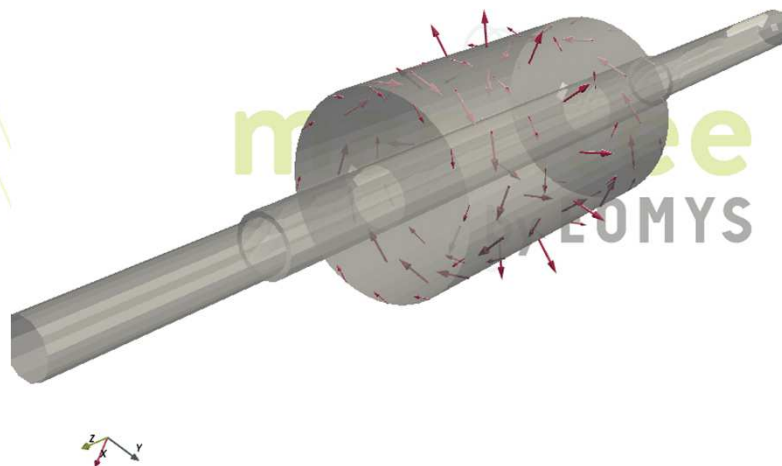


#10 « Skewing reduces magnetic noise and vibration levels »

Skewing can increase the noise level due to magnetic forces. This may be due to side effects such as axial forces, or excitation of longitudinal modes due to force variations along the axis.

There can be different optimum skew angles to reduce cogging torque, torque ripple and magnetic noise.

Rotor resultant OFS
at 10 (rpm), H60 (Fmax=0.09056 N)



10/10

Interested in learning more about e-NVH?

Next webinar on Manatee e-NVH software planned 20th April 2023

<https://manatee.eomys.com/manatee-webinars/>

Next technical training on e-NVH planned 23-25th May 2023 at EOMYS office

<https://www.training.eomys.com/>

